



Large-Scale Testing of Steel Reinforced Concrete (SRC) Coupling Beams

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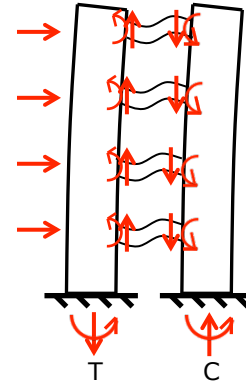
Presentation Outline

- Background
- Motivation
- Specimen Design
- Testing Program
- Test Results
- Backbone Modeling
- Conclusions & Recommendations



Background – Coupling Beams

- RC coupling beams
 - Diagonally-reinforced
 - Concrete-encased structural steel
- Primary functions
 - Added strength & stiffness
 - energy dissipation
- Primary issues
 - Detailing issues (ductility)
 - Modeling (e.g., backbone relation)



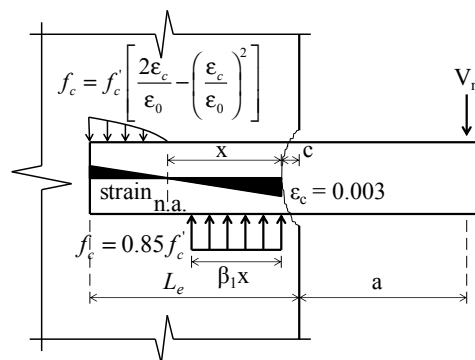
Diagonally-Reinforced



Concrete-Encased Steel

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Embedment Model



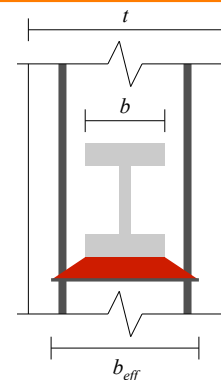
Marcakis & Mitchell (1980)* :

$$V_n = \frac{0.85 f_c' b_{eff} (l_e - c)}{1 + 3.6 \left(\frac{e}{(l_e - c)} \right)}$$

Mattock & Gaafar (1982)* :

$$V_n = 4.5 \sqrt{f_c'} \left(\frac{t}{b} \right)^{0.66} \beta_1 b (l_e - c) \left(\frac{0.58 - 0.22 \beta_1}{0.88 + (a + c) / (l_e - c)} \right)$$

*Modified to include interface spalling per Harries et al (2000)



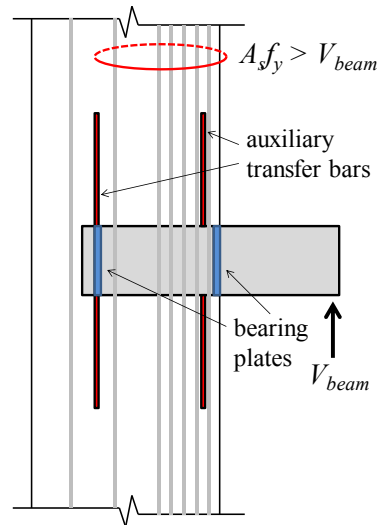
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AISC 2010 Seismic Provisions

- Flexural capacity using strain compatibility or plastic analysis
- Shear capacity using

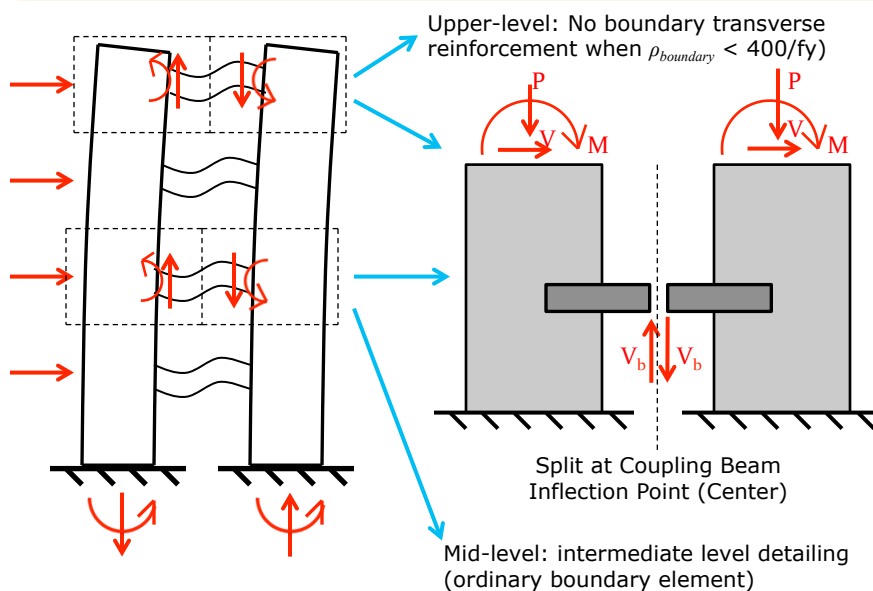
$$V_{comp} = 1.1R_y V_{steel} + 1.56V_{RC}$$
- Initial stiffness using $0.35Ig$
- Embedment length consistent with Mattock and Gaafar (1982)
- Transfer bars and bearing plates required
- Vertical boundary steel:

$$A_s f_y \geq V_{n,beam}$$



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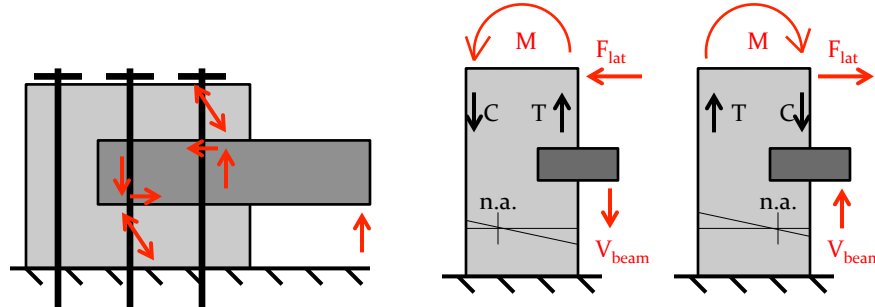
Test Sub-Assembly



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Motivation

- Large-scale SRC beam
- Realistic boundary conditions (load paths)
 - Wall strain gradient across connection



Embedment into reaction block:

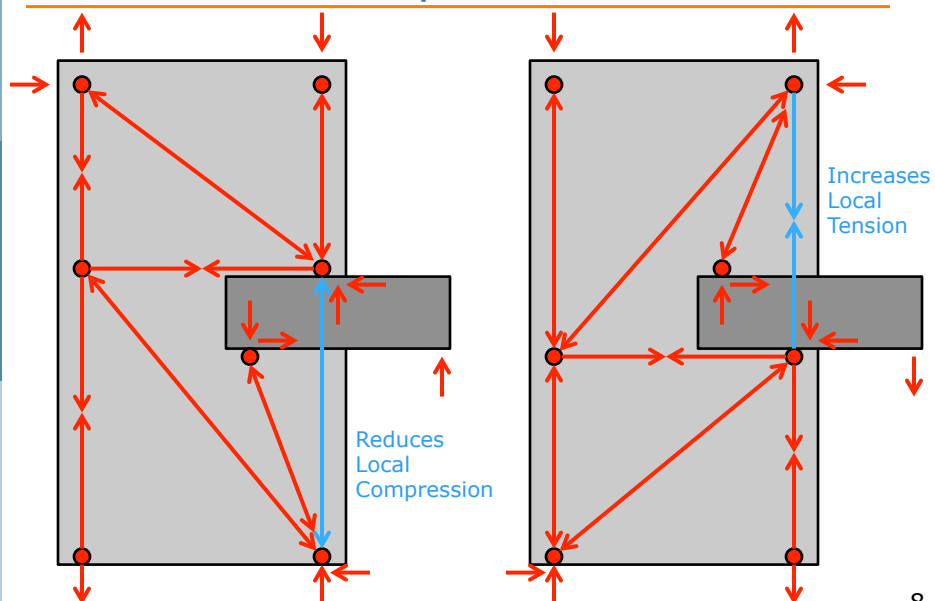
- No strain gradient
- Load path satisfied

Embedment into wall boundary:

- Strain gradient at embedment
- Imposes demands on wall

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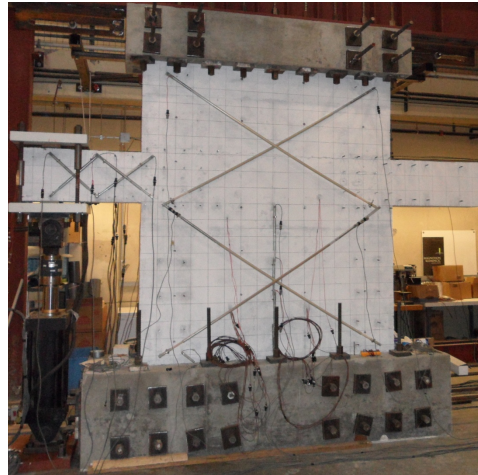
Motivation – Impact of Load Paths



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Testing Program Overview

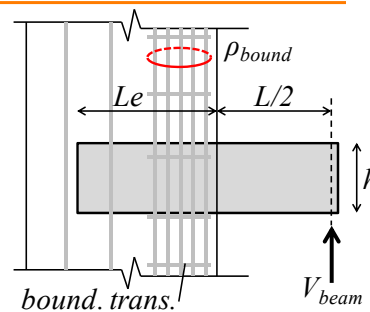
- Two test specimens
- Each specimen
 - One wall
 - Two coupling beams, one on each side
- Coupling beam tests
 - Individually with wall loads applied
- Second specimen designed after testing completed on first specimen



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Summary of Test Variables

- Beam 1: Long embedment (conservative design)
- Beam 2: Shorter embedment
- Beam 3: Shorter aspect ratio
- Beam 4: No boundary confinement, $\rho_{bound} < 400/f_y$

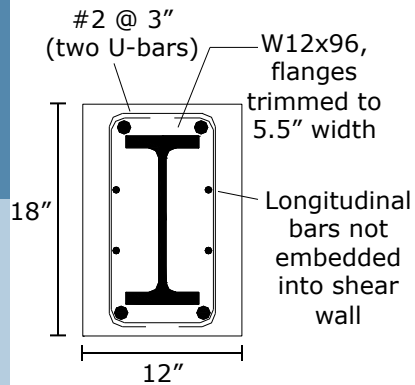


	$\alpha_{beam} = L/h$	L_e	$\rho_{bound.}$	bound. trans.
Beam 1 (3.33-32-6C)	3.33	32"	0.024 (14#6)	#2@4"
Beam 2 (3.33-24-7C)	3.33	24"	0.033 (14#7)	#2@4"
Beam 3 (2.40-26-5C)	2.40	26"	0.017 (14#5)	#2@4"
Beam 4 (3.33-24-3NC)	3.33	24"	0.006 (14#3)	none

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Coupling Beam

- Flexure-controlled
- ~1/2-scale W24x250



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Shear Wall Boundary



Ordinary boundary element

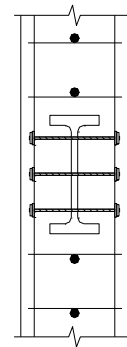
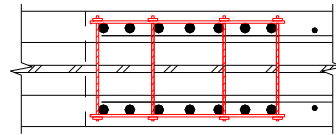


No boundary Confinement

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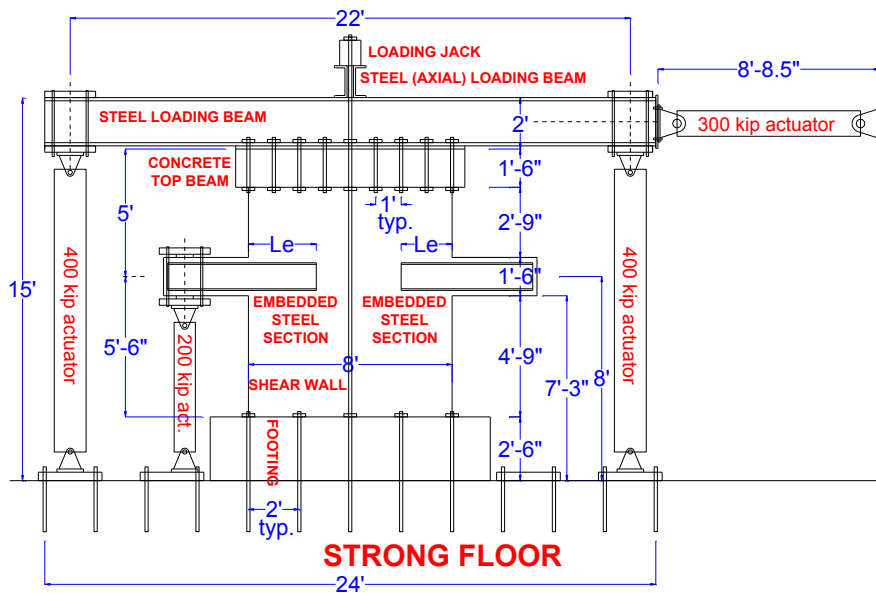
Embedment Detailing

- Pre-drilled holes in web of steel section
- Threaded rods and side plates to maintain boundary confinement

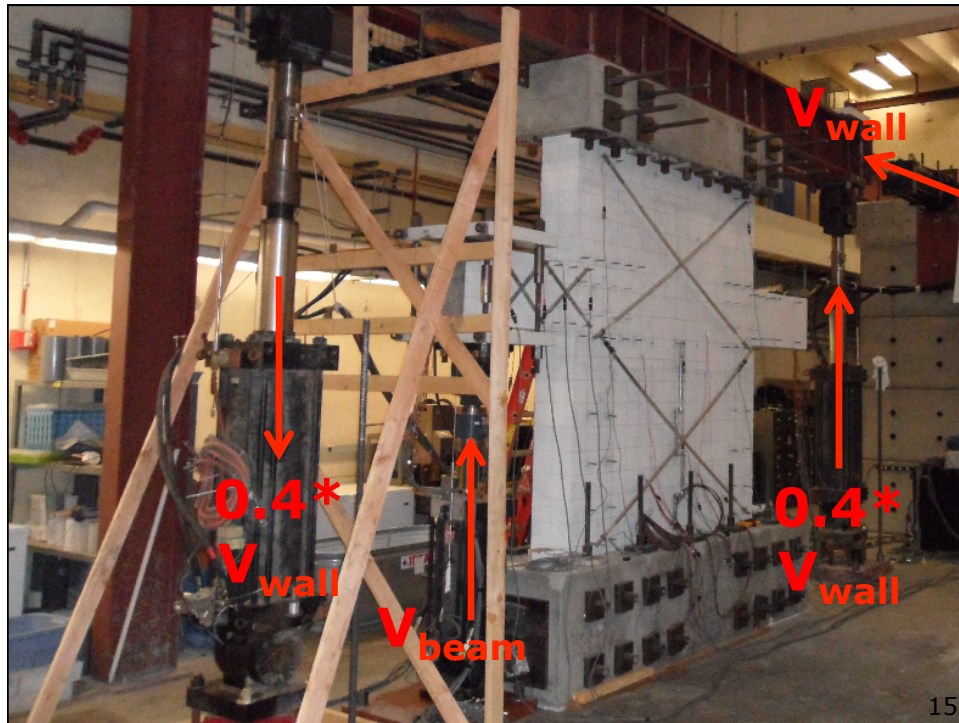


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Test Set-Up



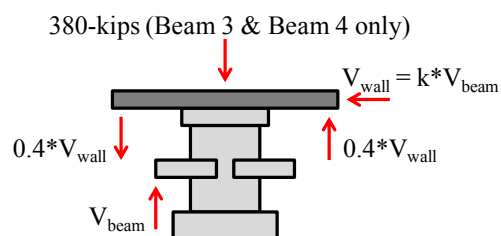
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Wall Loading

- Proportional loading: V_u and M_u
- Wall moment demands at connection
 - Beam 1: Exceeded cracking moment (low moment, long L_e)
 - Beam 2: Approached yield moment (high moment, short L_e)
- Wall moment demands at connection
 - Beam 3 and Beam 4: Similar to Beam 2



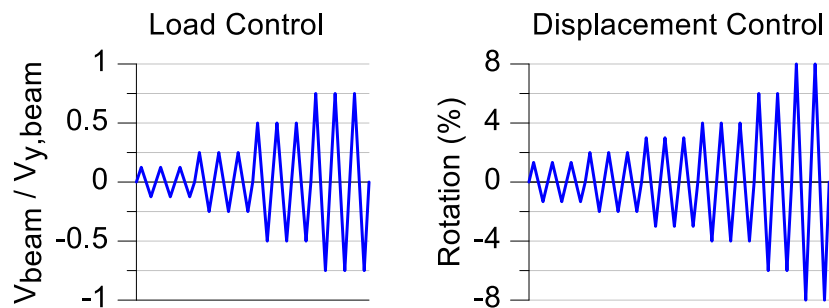
$$k = V_{\text{wall}} / V_{\text{beam}} =$$

	(+), Up	(-), Down
Beam 1	0.5	0.5
Beam 2	1.25	1.25
Beam 3	1.0	0.5
Beam 4	1.0	0.5

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Testing Protocol

- Reversed cyclic loading
- 3 cycles at each level up to 4%, then 2 cycles
- Load-controlled to $(+/-) \frac{3}{4} V_{yield}$, then displacement-controlled



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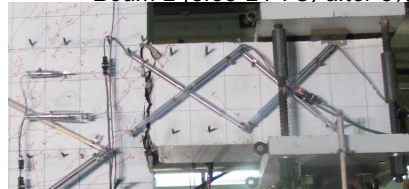
Observed Damage (Beams 1 & 2)

- Concentrated at beam-wall interface

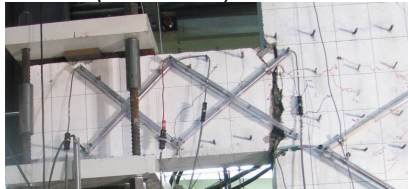
Beam 1 (3.33-32-6C) after 3%



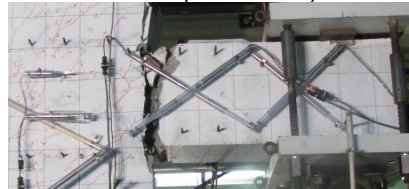
Beam 2 (3.33-24-7C) after 3%



Beam 1 (3.33-32-6C) after 6%

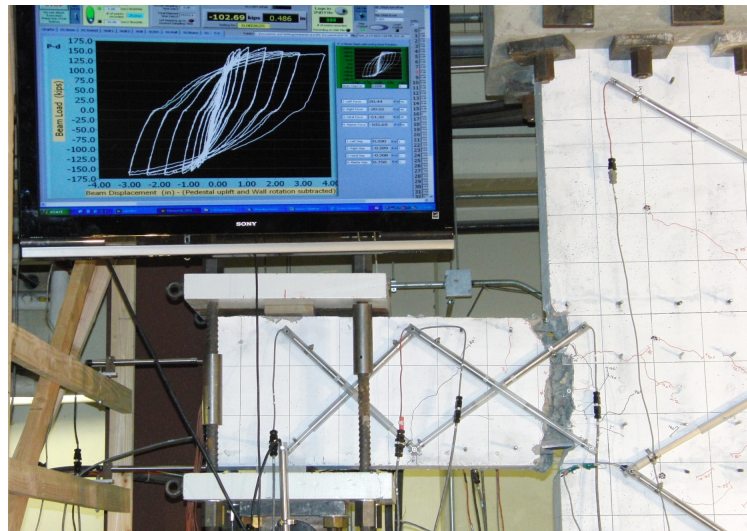


Beam 2 (3.33-24-7C) after 6%



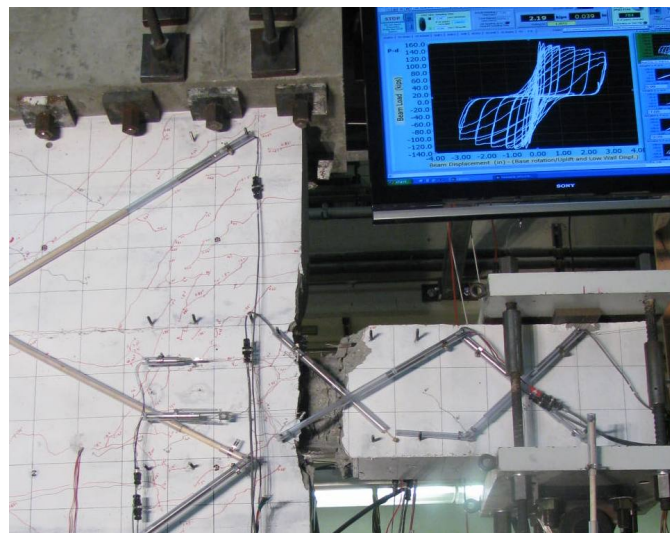
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Beam 1: 3.33-32-6C (end of test)



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Beam 2: 3.33-24-7C (end of test)



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Observed Damage (Beams 3 & 4)

- Included embedment damage

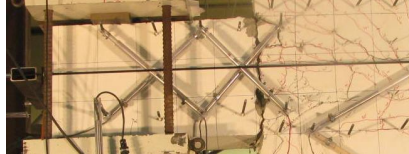
Beam 3 (2.40-26-5C) after 3%



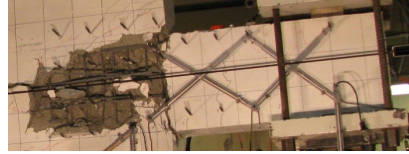
Beam 4 (3.33-24-3NC) after 3%



Beam 3 (2.40-26-5C) after 6%

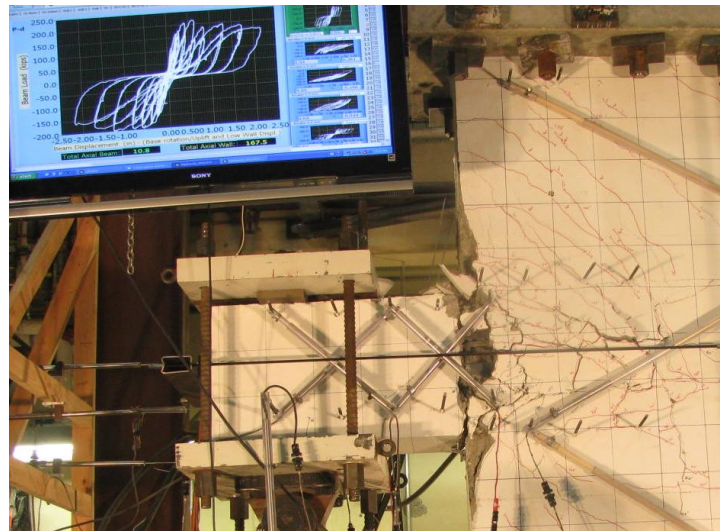


Beam 4 (3.33-24-3NC) after 6%



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2.40-26-5C (end of test)



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3.33-24-3NC (end of test)



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Observed Damage

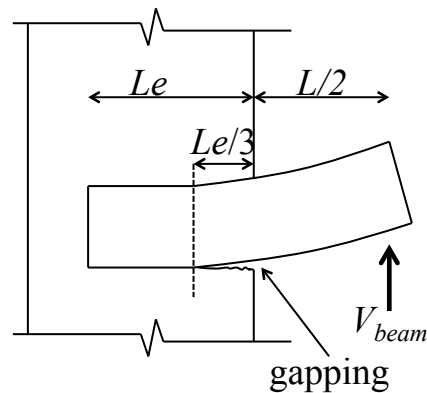


Photo showing significant gapping between flange and concrete (3.33-24-7C)

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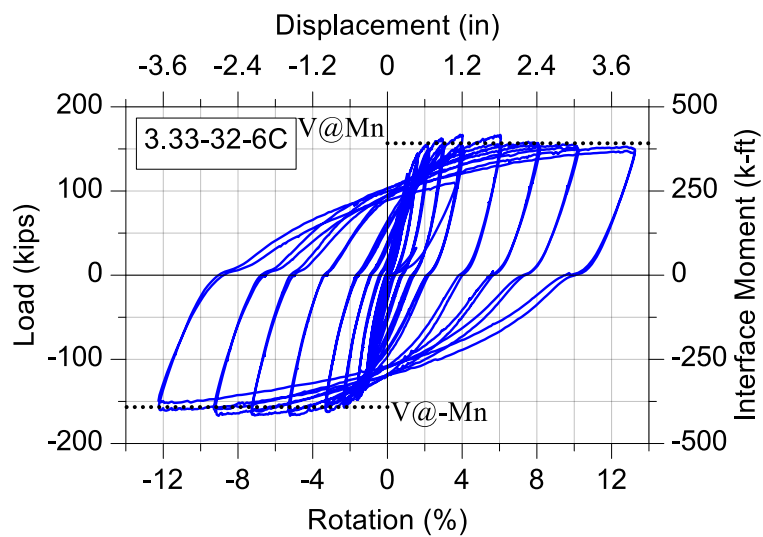
Modeling Recommendation

- Harris et al (2000) recommend taking the effective fixity point at $Le/3$ inside the beam-wall interface for modeling purposes



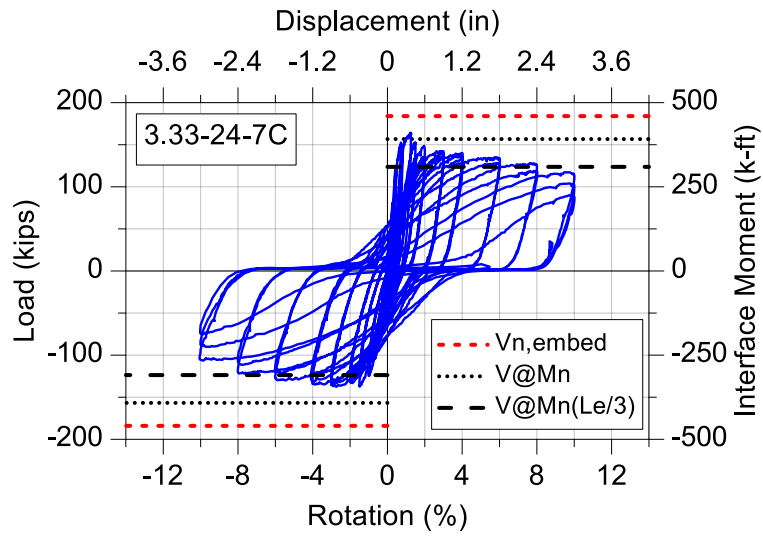
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Load-Displacement



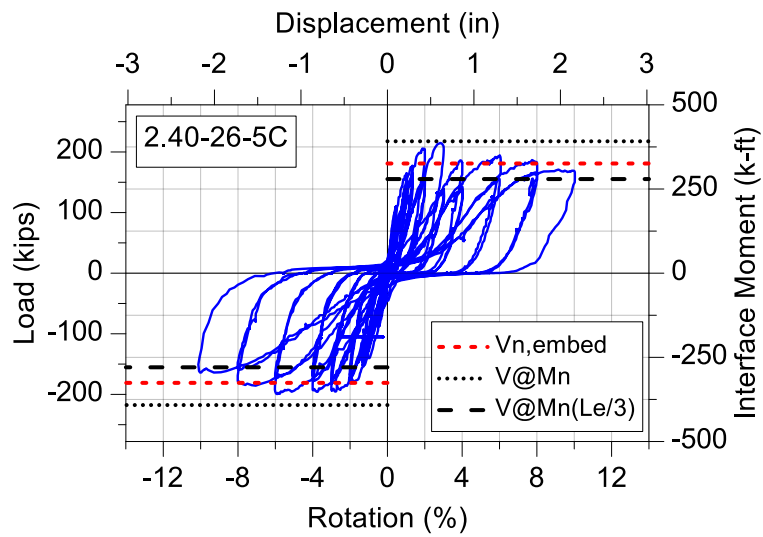
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Load-Displacement



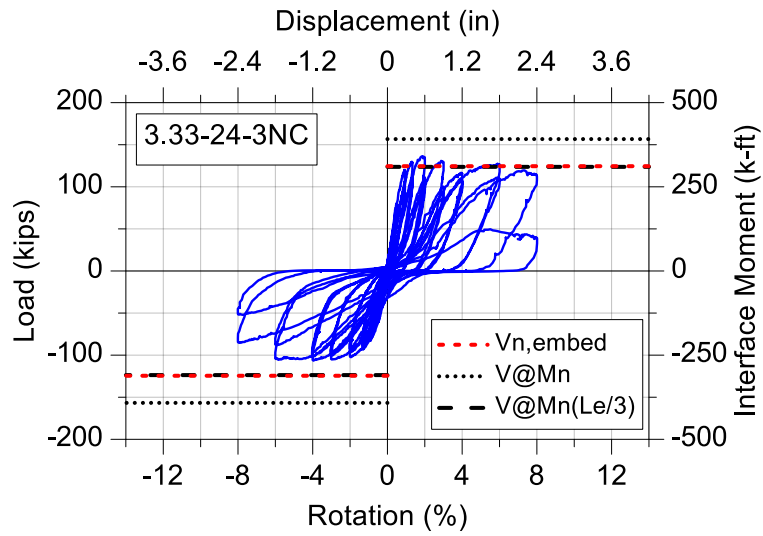
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Load-Displacement



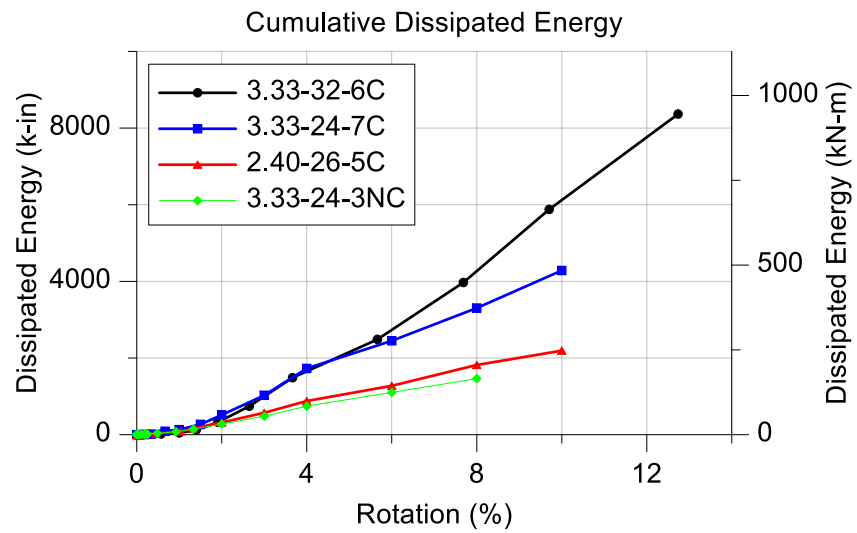
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Load-Displacement



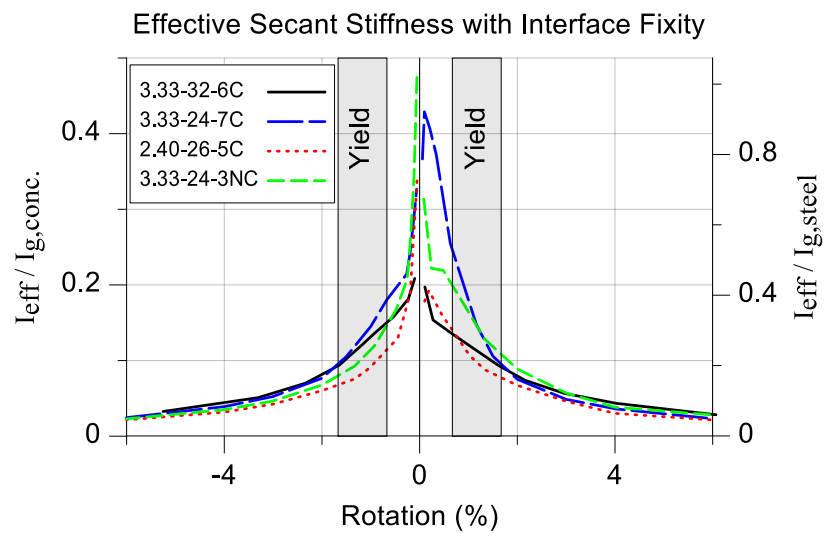
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Test Results



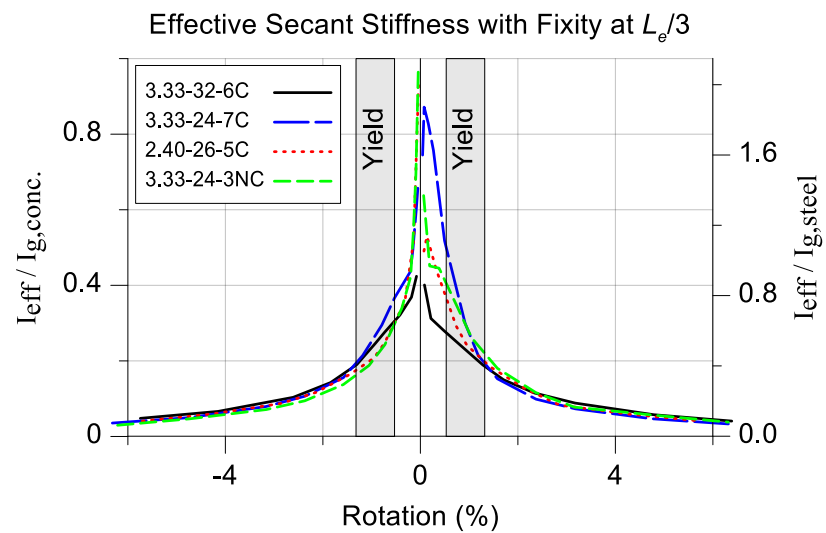
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Test Results



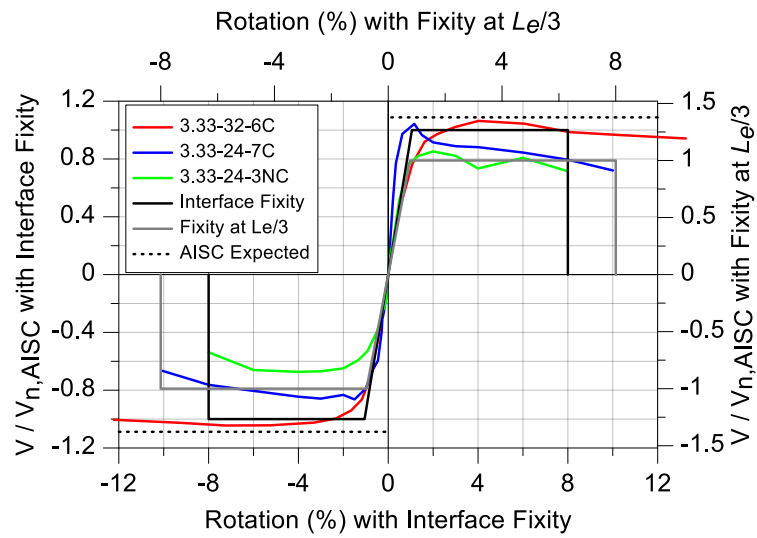
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Test Results



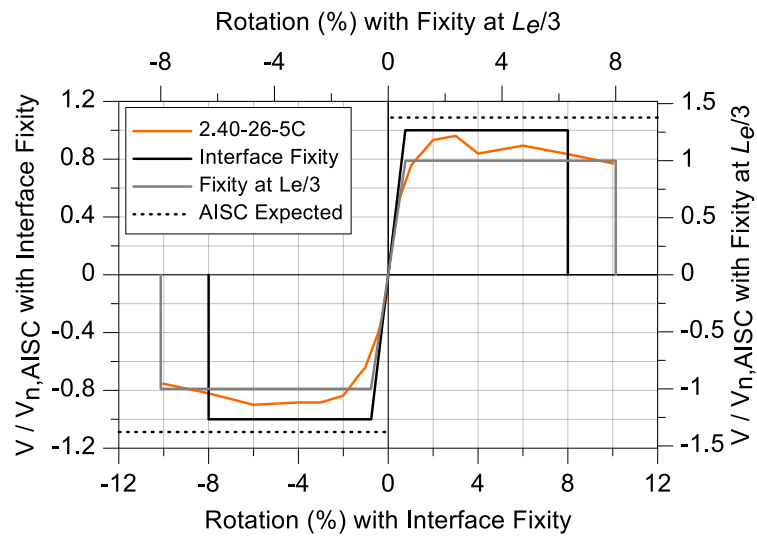
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Backbone



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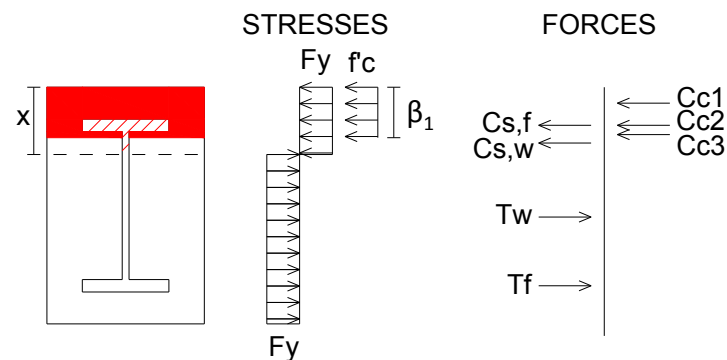
Backbone



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Recommendation(1) - Capacity

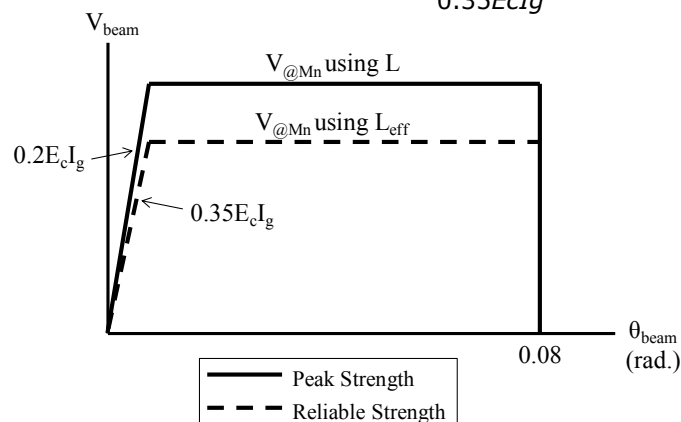
- Flexural capacity, M_n , determined using plastic section analysis with the design steel stress, F_y , and a Whitney stress block
- Probable flexural capacity for computing embedment length, $M_{n,pr}$, considers expected steel stress $R_y \cdot F_y$



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Recommendation(2) - Backbone

- For peak shear:
 - Interface fixity, use clear span, L
 - Use initial stiffness $0.2EcI_g$
- For reliable shear:
 - Effective fixity, use $L_{eff} = L + L_e/3$
 - Use initial stiffness $0.35EcI_g$



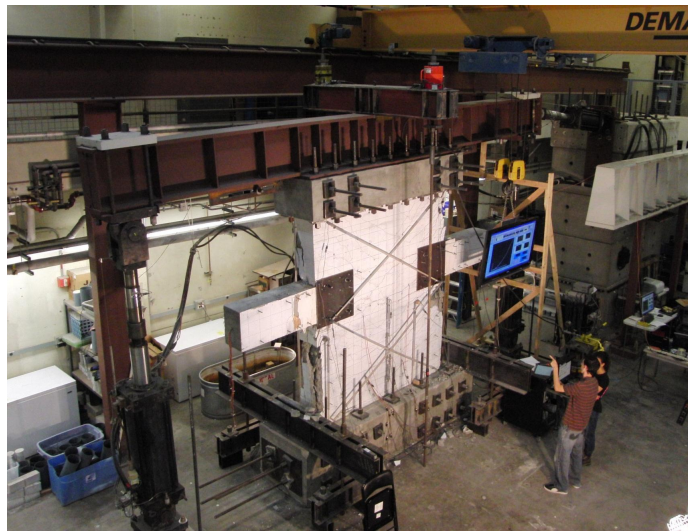
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Recommendation(3) - Embedment

- Embedment length per Marcakis and Mitchell (1980), Mattock and Gaafar (1982), or AISC 2010 Seismic Provisions
 - Use design f'_c
- Transfer bars and bearing plates
 - Not needed if sufficient quantity of wall boundary vertical reinforcement, i.e. Beam 1, Beam 2
 - May improve embedment performance if insufficient embedment length or wall boundary vertical reinforcement, i.e. Beam 3, Beam 4

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Shear Wall Testing



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Objectives

- Typical wall tests:
 - Thin walls, i.e. 6"
 - Special boundary elements, $s=4"$
- This specimen:
 - Thick wall
 - 12" test specimen, 24" thick full-scale
 - Intermediate confinement, i.e. ordinary boundary element
 - $s=4"$ test specimen, $s=8"$ full scale

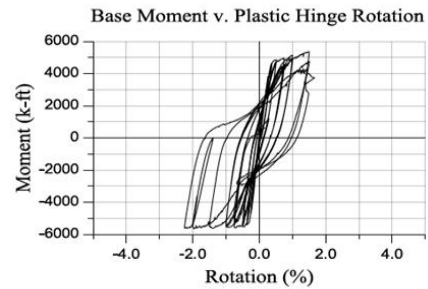
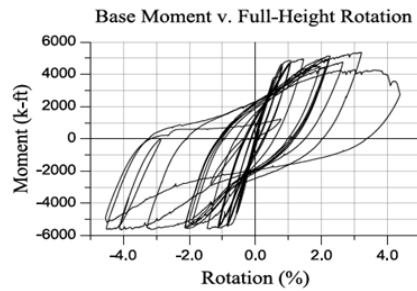
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Shear Wall Testing



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Shear Wall Testing



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Thank you

- Questions?

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